

Date Issued	Friday, 16 May 2025
Job No	DT 241201
Site	8 HOCKING PLACE, ADELAIDE
Client	SUE CRAFTER
Proposed	14-STOREY RESIDENTIAL DEVELOPMENT

Hydrological Analysis

Structural **S**ystems Pty Ltd 108 Wright Street, Adelaide SA 5000

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STRUCTURAL SYSTEMS

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DT24/201 8 Hocking place, Adelaide, Sote locate: -34.9338, 138.5952

Design a single or muliti rainwater tank locate at higher floor to provide reuseable water and overflow to underground tank; underground tank catch balconies water and pump to street water table.

Therefore, separate balconies rainwater and roof's rainwater to provide clear water for reuse purpose.

As required by PlanSA POI.I, the highest point of natural ground level at the primary street boundary where there is no kerb, and Council of any Adelaide required south side as lower's point.

Considered balconies contohnent: 2:1

Catchment Areas Level 1 ~ level 10 = 13.7m2 x 10 = 137m2 Level 11 ~ level 13 = 10, 4m2 x 3 = 3/,2m2

total = 168.2m2

Internal floor over :

Level 1 ~ 10 = type 1 = 52 m2 type 2 :54m2 Sum: 160m2 X 10 = 1600m2 type 3 :54m2

Level 11~13: type 1:82m2 type 2 = 82m2 Sum = 164m2x3 = 492m2

total 2092 m2 Roof: 250m2+1/2x(250m2xtan(5))=260m2



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A total rainwater storage capacity of 3000 L is proposed for this development, with a preferred location at level 13 to take advantage of gravity-fed distribution where possible. The system may comprise a single 3000 L tank or, if space and structural consideration require, 1000 L X 3 tank installed in parallel to achieve the same capacity.

The rainwater tanks will collect water from roof catchments via a dedicated rainwater pipe system. First flush diverters and appropriate filtration measure will be installed upstream to ensure the water quality is suitable for non-potable use, such as toilet flushing, irrigation, and general cleaning.

To manage overflow during periods of high rainfall, any excess water from the tanks on level 13 will gravity-drained via dedicated overflow pipe to the underground tank located at ground floor. This undergrand tank may be used for second storage or stormwater detention.

Adopt defention 4.31 m3 as calculation.

Our underground tank 13.64KL Which more than 4.31 m³
Outlet control as pump rate 24/5
Council require less than 1545 OK!

Rain water tanks

Installation

In order to fully extend the life of your concrete rain water tank, site preparation is essential:

- Excavate to the required depth plus 75mm (or more if required to achieve a fall from gutter height) and then back-fill with a layer of 10mm-12mm gravel or screenings. The tank will then be placed directly onto this level base.
- Ensure the gutter outlet is above the tank inlet.
- Check delivery access with Ri-Industries.
- A minimum height clearance of 8 metres is required when unloading.
- 4.7 metres is needed for the truck to pass under trees and overhead power lines.
- 4 metres clearance is required between gate posts.
- Please highlight the position of any underground drains or cables. Trucks will not drive over any concrete or sealed areas without indemnity being signed (including all foundations).
- Please ensure the unloading site is level.
- Ri-Industries strongly recommends your tank not be left empty for extended periods.
- If any tank is partially buried more than 900mm in the ground there is a possibility that it may float unless precautions are taken. We suggest that the tank is filled with water immediately after placement to at least ground level, until the back-fill soil has compacted.
- If you have any doubts regarding your installation a site inspection can be arranged.

Please also note that:

- Each above ground tank is painted and includes a 75mm diameter drain outlet made of brass. The overflow is ready to take a 90mm PVC stormwater pipe. Male brass fittings can be fitted in the tank depending on customer requirements eg. for fire fighting purposes.
- Underground rain water tanks can be installed down to a maximum of 2 metres below the ground but this requires riser pipes to allow access at ground level and a heavy duty concrete cover.

Specifications

- Specifications can be forwarded through to Council/engineers upon request.
- Four sizes of tank are available in both above ground and underground options.

Tank capacity	Diameter	Height	Weight	
5,000 litres	1930mm	2240mm	2.97 tonne	ABOVE diam → diam → to ie
9,090 litres	2440mm	2460mm	3.9 tonne	GROOND ₹
13,640 litres	2870mm	2440mm	4.9 tonne	
22,730 litres	3450mm	2740mm	7.3 tonnes	GROUND diam → diam → diam →
*Heights and weights showr	n are for tank only.			\

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IFD Design Rainfall Intensity (mm/h)

Issued: 16-May-25

Location Label:

Requested Latitude -34.9338 Longitude 138.5953 Nearest gri Latitude 34.9375 (S Longitude 138.5875 (E)

	Д	nnual Exce	edance Pro	bability (AE	P)			
Duration	Duration in n	63.20%	50%	20%	10%	5%	2%	1%
1 min	1	77.7	88.4	125	154	184	229	268
2 min	2	68.3	77.5	109	134	161	202	236
3 min	3	60.9	69.1	97.6	120	144	179	210
4 min	4	55.1	62.5	88.5	108	130	162	190
5 min	5	50.4	57.3	81.2	99.6	119	149	174
10 min	10	36.6	41.6	59.1	72.5	86.9	108	126
15 min	15	29.4	33.5	47.6	58.4	70	87	101
20 min	20	25	28.4	40.4	49.6	59.4	73.9	86.2
25 min	25	21.9	24.9	35.4	43.4	52	64.7	75.6
30 min	30	19.6	22.3	31.6	38.8	46.5	57.9	67.6
45 min	45	15.2	17.3	24.5	30	36	44.8	52.4
1 hour	60	12.7	14.4	20.3	24.9	29.8	37.2	43.4
1.5 hour	90	9.76	11.1	15.6	19	22.8	28.3	33.1
2 hour	120	8.08	9.15	12.8	15.7	18.7	23.2	27.1
3 hour	180	6.19	6.99	9.76	11.9	14.1	17.5	20.3
4.5 hour	270	4.72	5.32	7.39	8.97	10.6	13.1	15.2
6 hour	360	3.89	4.38	6.06	7.33	8.67	10.6	12.3
9 hour	540	2.95	3.31	4.56	5.49	6.47	7.86	9.02
12 hour	720	2.41	2.71	3.71	4.46	5.23	6.33	7.22
18 hour	1080	1.81	2.03	2.76	3.3	3.86	4.62	5.24
24 hour	1440	1.47	1.64	2.23	2.65	3.09	3.68	4.16
30 hour	1800	1.24	1.39	1.88	2.23	2.59	3.08	3.46
36 hour	2160	1.09	1.21	1.63	1.93	2.24	2.65	2.97
48 hour	2880	0.872	0.973	1.3	1.53	1.77	2.09	2.33
72 hour	4320	0.638	0.709	0.939	1.1	1.26	1.48	1.64
96 hour	5760	0.51	0.566	0.743	0.865	0.987	1.15	1.27
120 hour	7200	0.43	0.475	0.619	0.718	0.814	0.94	1.04
144 hour	8640	0.374	0.413	0.534	0.616	0.694	0.798	0.877
168 hour	10080	0.334	0.368	0.472	0.541	0.607	0.694	0.76

Estimate the discharge flow to outlet point - FULL SITE

Catchment analysis

Total Catchme Roof Paving Pervious area	nt Area =		250 250 0 0	m_2^2	equivalent equivalent equivalent		100.0 ° 0.0 ° 0.0 °	%	C10 0.9 0.75 0.1	
Cy = C1	10*Fy									
Design ARI	1	2	5	10	20	40	50	60	80	100
Fy	0.8	0.85	0.95	1	1.05	1.13	1.15	1.17	1.19	1.2
Equivalent CA	at ARI (y	ears)								
-	1	2	5	10	20	40	50	60	80	100
(m^2) CA =	180	191	214	225	236	250	250	250	250	250
(ha) CA =	0.018	0.019	0.021	0.023	0.024	0.025	0.025	0.025	0.025	0.025
Cequiv =	0.72	0.77	0.86	0.90	0.95	1.00	1.00	1.00	1.00	1.00

Estimate discharge rate for design area for 1, 5,10,20 and 100 years ARI storm event (L/s)

Q = 0.000278*CAI (L/s) Rational Method

Storm Duration (min)	I ₁ (63.2%AEP) (mm/hr)	Outflow 1y ARI	I ₅ (20%AEP) (mm/hr)	Outflow (L/s) 5y ARI	I ₁₀ (10%AEP) (mm/hr)	Outflow (L/s) 10y ARI	(5%AEP)	Outflow (L/s) 20y ARI	I ₁₀₀ (1%AEP) (mm/hr)	Outflow (L/s) 100y AR
5	50.40	2.52	81.20	4.83	99.60	6.23	119.00	7.82	174.00	12.09
10	36.60	1.83	59.10	3.51	72.50	4.53	86.90	5.71	126.00	8.76
15	29.40	1.47	47.60	2.83	58.40	3.65	70.00	4.60	101.00	7.02
20	25.00	1.25	40.40	2.40	49.60	3.10	59.40	3.90	86.20	5.99
25	21.90	1.10	35.40	2.10	43.40	2.71	52.00	3.42	75.60	5.25
30	19.60	0.98	31.60	1.88	38.80	2.43	46.50	3.05	67.60	4.70
45	15.20	0.76	24.50	1.46	30.00	1.88	36.00	2.36	52.40	3.64
60	12.70	0.64	20.30	1.21	24.90	1.56	29.80	1.96	43.40	3.02
90	9.76	0.49	15.60	0.93	19.00	1.19	22.80	1.50	33.10	2.30
120	8.08	0.40	12.80	0.76	15.70	0.98	18.70	1.23	27.10	1.88
180	6.19	0.31	9.76	0.58	11.90	0.74	14.10	0.93	20.30	1.41
270	4.72	0.24	7.39	0.44	8.97	0.56	10.60	0.70	15.20	1.06
360	3.89	0.19	6.06	0.36	7.33	0.46	8.67	0.57	12.30	0.85
540	2.95	0.15	4.56	0.27	5.49	0.34	6.47	0.42	9.02	0.63
720	2.41	0.12	3.71	0.22	4.46	0.28	5.23	0.34	7.22	0.50
1080	1.81	0.09	2.76	0.16	3.30	0.21	3.86	0.25	5.24	0.36
1440	1.47	0.07	2.23	0.13	2.65	0.17	3.09	0.20	4.16	0.29
1800	1.24	0.06	1.88	0.11	2.23	0.14	2.59	0.17	3.46	0.24
2160	1.09	0.05	1.63	0.10	1.93	0.12	2.24	0.15	2.97	0.21
2880	0.87	0.04	1.30	0.08	1.53	0.10	1.77	0.12	2.33	0.16
4320	0.64	0.03	0.94	0.06	1.10	0.07	1.26	0.08	1.64	0.11

Estimate the discharge flow to outlet points POST development (Roof, Balconies) southern section - proposed up stream direct to Piccadilly Road - Area1

Catchment analysis

Total Catchmer 1st grade pavir 2nd grade pavi Pervious area	ng		428.1 0	m ² m ² m ² m ²	equivalent equivalent equivalent		100.0 9 0.0 9 0.0 9	%	C10 0.9 0.75 0.1		
Cy = C1	0*Fy										
Design ARI	1	2	5	10	20	40	50	60	80	100	(years)
Fy	8.0	0.85	0.95	1	1.05	1.13	1.15	1.17	1.19	1.2	,
Equivalent CA	at ARI (y	ears)									
	1	2	5	10	20	40	50	60	80	100	
(m^2) CA =	308	327	366	385	405	428	428	428	428	428	
(ha) CA =	0.031	0.033	0.037	0.039	0.040	0.043	0.043	0.043	0.043	0.043	
Cequiv =	0.72	0.77	0.86	0.90	0.95	1.00	1.00	1.00	1.00	1.00	

Estimate discharge rate for design area for 1, 5,10,20 and 100 years ARI storm event (L/s)

Q = 0.000278*CAI (L/s) Rational Method

Storm Duration (min)	I ₁ (63.2%AEP) (mm/hr)	Outflow 1y ARI	I ₅ (20%AEP) (mm/hr)	Outflow (L/s) 5y ARI	I ₁₀ (10%AEP) (mm/hr)	Outflow (L/s) 10y ARI	I ₂₀ (5%AEP) (mm/hr)	Outflow (L/s) 20y ARI	I ₁₀₀ (1%AEP) (mm/hr)	Outflow (L/s) 100y ARI	Vol	Est Ponding /detention Vol (m3)
5	50.40	4.32	81.20	8.26	99.60	10.67	119.00	13.38	174.00	20.71	6.21	3.87
10	36.60	3.14	59.10	6.01	72.50	7.77	86.90	9.77	126.00	15.00	9.00	4.31
15	29.40	2.52	47.60	4.84	58.40	6.26	70.00	7.87	101.00	12.02	10.82	3.78
20	25.00	2.14	40.40	4.11	49.60	5.31	59.40	6.68	86.20	10.26	12.31	2.93
25	21.90	1.88	35.40	3.60	43.40	4.65	52.00	5.85	75.60	9.00	13.50	1.77
30	19.60	1.68	31.60	3.22	38.80	4.16	46.50	5.23	67.60	8.05	14.48	0.41
45	15.20	1.30	24.50	2.49	30.00	3.21	36.00	4.05	52.40	6.24	16.84	0.00
60	12.70	1.09	20.30	2.07	24.90	2.67	29.80	3.35	43.40	5.17	18.59	0.00
90	9.76	0.84	15.60	1.59	19.00	2.04	22.80	2.56	33.10	3.94	21.27	0.00
120	8.08	0.69	12.80	1.30	15.70	1.68	18.70	2.10	27.10	3.23	23.22	0.00
180	6.19	0.53	9.76	0.99	11.90	1.27	14.10	1.59	20.30	2.42	26.09	0.00
270	4.72	0.40	7.39	0.75	8.97	0.96	10.60	1.19	15.20	1.81	29.31	0.00
360	3.89	0.33	6.06	0.62	7.33	0.79	8.67	0.98	12.30	1.46	31.62	0.00
540	2.95	0.25	4.56	0.46	5.49	0.59	6.47	0.73	9.02	1.07	34.78	0.00
720	2.41	0.21	3.71	0.38	4.46	0.48	5.23	0.59	7.22	0.86	37.12	0.00
1080	1.81	0.16	2.76	0.28	3.30	0.35	3.86	0.43	5.24	0.62	40.41	0.00
1440	1.47	0.13	2.23	0.23	2.65	0.28	3.09	0.35	4.16	0.50	42.78	0.00
1800	1.24	0.11	1.88	0.19	2.23	0.24	2.59	0.29	3.46	0.41	44.47	0.00
2160	1.09	0.09	1.63	0.17	1.93	0.21	2.24	0.25	2.97	0.35	45.81	0.00
2880	0.87	0.07	1.30	0.13	1.53	0.16	1.77	0.20	2.33	0.28	47.92	0.00
4320	0.64	0.05	0.94	0.10	1.10	0.12	1.26	0.14	1.64	0.20	50.59	0.00

Q20pre - 5mins = 7.82 (L/s)

Stormwater Calculations



Report for

Project Details

Project Name	DT 241201	
User Email		
Web files link		
Site Area (m2)	250 Project ID	544
Planning number		
Development type	Multi unit development (apartment building)	
Existing site details	Commercial (including car parks)	
Street address	8 Hocking Pl, Adelaide SA 5000, Australia	

Results

VOLUME	FLOW	QUALITY	EFFICIENCY
Objective: Harvest or infiltrate stormwater	Objective: Control peak discharge flows	Objective: Improve stormwater runoff water quality	Objective: Increase drought resilience
Target: No more than a 10% increase in runoff volume	Target less than or equal to zero. If greater than zero this is the additional Site Storage Requirement (SSR) volume required	Target: Achieve a score of 100 or more	Target: Achieve greater than 25% potable water use reduction
VOLUME RESULT	FLOW RESULT	QUALITY RESULT	EFFICIENCY RESULT
-84.7 % change in annual average volume	-8.0 m ³ of additional site storage required	206 Pollution reduction score (out of 100)	29.8 % water saving

VOLUME PASSES FLOW PASSES QUALITY PASSES EFFICIENCY PASSES

This project meets all of the policy objectives

Design Criteria

The development must be designed and constructed in accordance with the following:

Stormwater management measures selected are

This includes all impervious areas in the site connected to Council or Stormwater Authority drains. This excludes pervious areas like pervious paving, garden, gravel and lawn areas)

- •Raintank Volume = 13640 litres connected to 168m2 of roof, additional detention tank volume included = 5000 litres
- •Raintank Volume = 3000 litres connected to 260m2 of roof, additional detention tank volume included = 1000 litres

Conditions of approval

Rainwater Tanks

Total rainwater retention tank volume (L)	16640
Area of roof connected to rainwater tank (plumbed to household) (m ²)	428.0
Total rainwater detention tank volume (L)	6000.00
Rainwater tanks connected to	Toilet Laundry
Other rainwater tank end uses (L/day)	Irrigated Garden Area (m²)
Additional* Site Storage (m³)	*Site storage added adjacent to the legal point of discharge for peak flow detention or volume infiltration
Recycled water source	
Water tank reliability %	50.6
Rainwater tank overflow %	7.2

Water Efficiency Specifications

Basin WELS star rating	Default or unrated
Toilet WELS rating	> 4 Star WELS rating
Bath WELS star rating	Not Applicable
Washing Machine WELS star rating	> 6 Star WELS rating
Kitchen Taps WELS rating	> 4 Star WELS rating
Urinal WELS rating	> 4 Star WELS rating
Shower WELS star rating	3 Star WELS (> 7.5 but <= 9.0) (minimum requirement)
Dishwasher WELS star rating	> 3 Star WELS rating

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Project Design Specifications

Estimated Total Building Occupancy

Building Spaces

- •Apartments BCA Class 2 of 2092m2 with an average occupancy of 49.7 people
- •Shop, restaurant or retail BCA Class 6 of 52m2 with an average occupancy of 1.6 people
- •Office BCA Class 5 of 12m2 with an average occupancy of 0.4 people

Stormwater Quality Calculations	
Rainwater Tank Runoff reduction (%)	92.8
Rainwater Tank(s) Total Nitrogen (TN) reduction	882.6
Total Impervious Area (m²)	168.2, 260.0
Total Nitrogen (TN) % reduction (g/yr)	92.8
Water Quality Score (%)	206
Rainwater Used (kL)	190.8
Total demand (L/day)	1033.20
Roof Runoff (kL)	205.8
Rainwater Tank Overflow (kL)	14.8
Peak Flow Storage Requirement Cal	culations
FLOW reduction strategy	Volume retention and/or Infiltration
Catchment strategy used	On Site Retention (OSR) of volume to pre-development levels - Regime-in-balanc
Site Storage Calculations	
Base case (pre-development) fraction impervious (ratio)	0.90
Base case runoff coefficient	0.840
Post development detention	
requirement (Site Storage Requirement)	5% AEP (~1 in 20 ARI) - default industrial
Post development fraction impervious (ratio)	1.71
Post development runoff coefficient	1.688
Pre-development FLOW volume (m³)	3.5
Post-development FLOW volume (m³)	7.0

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FLOW Volume storage required for 'yield minimum' (m³)	
FLOW volume storage required for 'regime in balance' (m³)	3.5
On Site Retention (m³)	3.5
Permissible Site Discharge (PSD) (L/sec)	
Critical Storm Duration - the Catchment time of concentration - Tc(catchment) in minutes	30
Rainfall Depth (mm) for Critical Storm Duration - Tc (Catchment)	16.57
Rainfall intensity - i at Tc(catchment) (mm/h)	33.1
Site time of Concentration (min) - Tc(site)	10.0
Rainfall Depth (mm) for tc(site) - (IFD at Site Time of Concentration)	10.3
Rainfall intensity - i at tc(site) (mm/h)	61.80

Detention Calculator - Site Storage Requirement (SSR) - Uses rational method (Boyd's Equation)

Please note that this section is not applicable if Volume retention and/or Infiltration strategy is used

Storm Duration (mins)	Rainfall Depth (mm)	Peak Post Development flow (L/s)	Runoff Volume (m³)	Stored Volume (m³)
5				
10				
15				
30				
60				
120				

About In-Site Water

This report is generated by user inputs from the toolkit at In-Site Water. In-Site water is an online Integrated Water Management tool designed for use on smaller sites (less than 2 hectares) in Australia that need quick and accurate stormwater engineering answers. In-Site water is simple to use but provides robust stormwater design and engineering answers.

For enquiries, contact Water Sensitive SA <u>www.watersensitivesa.com</u>

Disclaimer

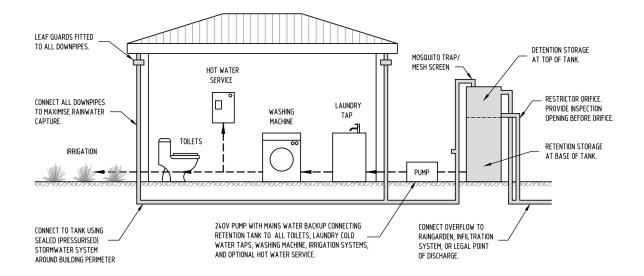
This guide is of a general nature only. Advice from a suitably qualified professional should be sought for your particular circumstances. Depending on each unique situation, there may be occasions where compliance is not achieved. The following dot points are outside the scope of this report, however it is critical that all designers consider the following:

- Manage expectations and risks around occasional surface water and ponding.
- Ensure that uncontrolled stormwater does not flow over property boundaries or otherwise cause a nuisance.
- Plan for major flood pathways locate away from, adapt (raise floors above predicted flood levels) and defend buildings against potential major flooding.
- Plan to reduce annual average damages and safety risks.
- Take into account local conditions such as slope, topography and soils (type, reactivity, permeability, water table level, salinity, dispersiveness, acid sulphate soils, etc.).
- Ensure that soil moisture and building clearance is considered in areas of reactive clays or where varying soil moisture levels could damage buildings, infrastructure or other constructions.
- For steeper sites, ensure the design includes geotechnical considerations such as slope stability with varying soil saturation levels.
- Compliance with other Australian Standards, laws, guidelines, regulations and Council requirements.

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Example details for this project (if applicable). Please see the *InSite Guide* for more details:

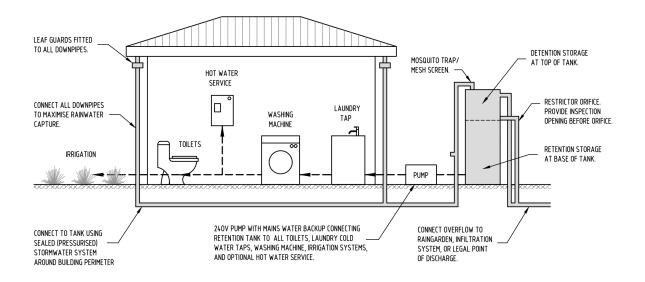


RETENTION TANK RETICULATION DETAIL

N.T.S.

NOTE: THE DESIGN AND INSTALLATION OF ALL STORMWATER SYSTEMS SHALL COMPLY WITH AS/NZS 3500.3:2018 "STORMWATER DRAINAGE".

Above: Balconies treatment



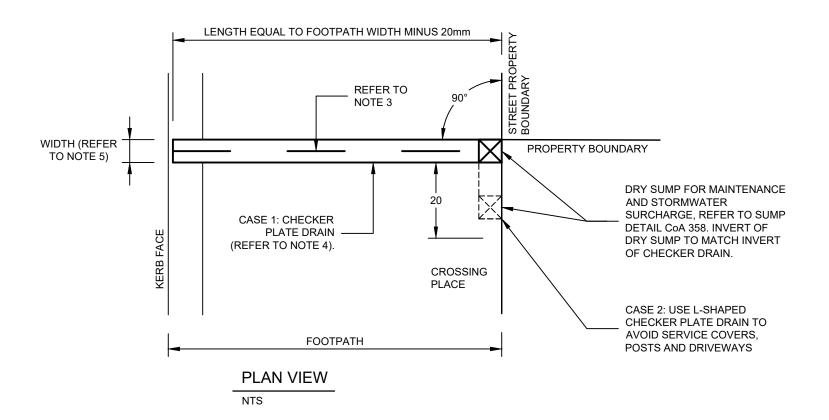
RETENTION TANK RETICULATION DETAIL

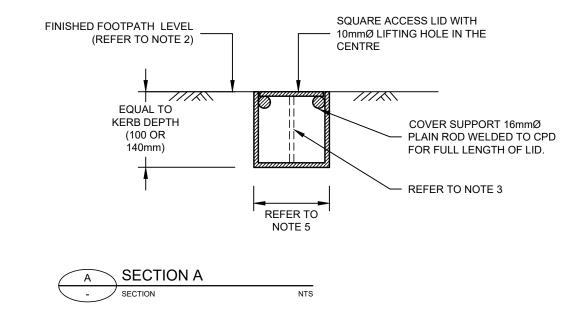
N.T.S.

NOTE: THE DESIGN AND INSTALLATION OF ALL STORMWATER SYSTEMS SHALL COMPLY WITH AS/NZS 3500.3:2018 "STORMWATER DRAINAGE".

Above: Propose roof treatment

PRIVATE PROPERTY



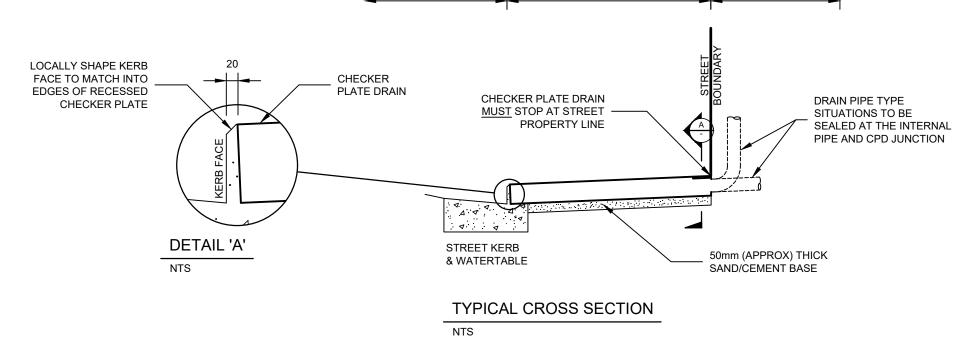


FOOTPATH

NOTES:

- CHECKER PLATE DRAIN (CPD) TO BE CONSTRUCTED OF 6mm THICK STEEL PLATE WITH STEEL CHECKER PLATE TOP ALL FULLY WELDED AND HOT DIPPED GALVANISED.
- 2. TOP OF CPD AND CHECKER PLATE ACCESS LID TO BE FLUSH WITH FOOTPATH SURFACE.
- ANY CPD WIDER THAN 300mm TO BE PROVIDED WITH A 500mm LONG INTERNAL STIFFENER, FULLY WELDED PLACED CENTRALLY AT KERB AND AT 500mm INTERVALS.
- 4. ALL CPD's TO BE INSTALLED PERPENDICULAR TO THE STREET PROPERTY BOUNDARY AND A MINIMUM OF 1.0 METRE CLEAR OF ANY CROSSING PLACE.
- 5. WIDTH DIMENSION TO BE EQUAL TO EXISTING CPD OR SIMILAR X-SECTIONAL AREA OF EXISTING PIPE, BUT NOT LESS THAN MINIMUM WIDTH.
- 6. CPD MINIMUM WIDTH 150mm.
- 7. L-SHAPED CPD MUST BE IN THE FOOTPATH WITHIN THE PROPERTY BOUNDARY ALIGNMENT DRAINING THAT PROPERTY
- 8. THIS DETAIL SHALL BE USED FOR MAINTENANCE PURPOSES ONLY, OR AS DIRECTED BY CoA REPRESENTATIVE.

NOTE: ALL COSTS ASSOCIATED WITH DISCHARGE OF PRIVATE PROPERTY STORMWATER TO COUNCIL INFRASTRUCTURE (UNDERGROUND STORMWATER MAIN OR KERB & WATERTABLE) SHALL BE THE RESPONSIBILITY OF THE PROPERTY OWNER.



ROAD RESERVE



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